

Innovative numerical methods for evolutionary partial differential equations and applications

Numerical validation of homogeneous multi-fluid models

Speaker: Dr. Phan Thi My Duyen
Joint work with: Prof. Giovanni Russo
and Prof. Sergey Gavriluk

University of Catania, Italy

21st February, 2023



Outline

- 1 Problem setup
- 2 Detailed numerical solution
- 3 Numerical tests
- 4 Multi-fluid models
- 5 Numerical comparison

Problem setup

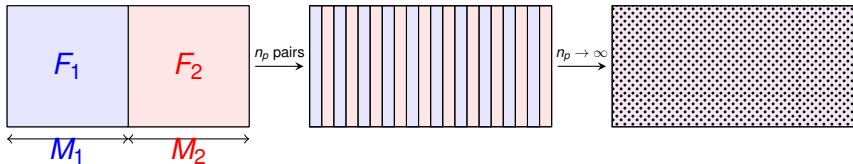


Figure: Homogeneous limit of a multi-fluid system.

Mass Lagrangian coordinates

We shall make use of the mass Lagrangian coordinates

$$\xi = \int_0^x \rho(z, t) dz = \int_0^X \rho_0(z) dz. \quad (1.1)$$

where x is the Eulerian coordinate, X is the initial position of fluid particles and $\rho_0(X)$ is the initial density.

The Lagrangian coordinates ξ corresponding to the position x is the mass from the origin of the tube $x_0 = 0$, to x .

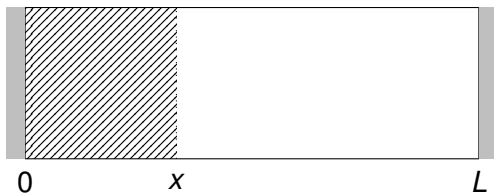


Figure: Describing the mass defined by Lagrangian coordinates



Outline

- 1 Problem setup
- 2 Detailed numerical solution**
- 3 Numerical tests
- 4 Multi-fluid models
- 5 Numerical comparison

Governing equations

Let us consider the Euler equations in Lagrangian coordinates

$$\frac{DU}{Dt} + \frac{\partial f(U)}{\partial \xi} = 0, \quad (2.1)$$



Governing equations

Let us consider the Euler equations in Lagrangian coordinates

$$\frac{DU}{Dt} + \frac{\partial f(U)}{\partial \xi} = 0, \quad (2.1)$$

where

$$U = \begin{pmatrix} V \\ u \\ E \end{pmatrix}, \quad f(U) = \begin{pmatrix} -u \\ p \\ up \end{pmatrix}. \quad (2.2)$$

$V = 1/\rho$ denotes the specific volume, $E = \frac{1}{2}u^2 + e$, where $e = e(V, p)$ denotes the specific internal energy.

The time derivative is Lagrangian derivative has the form

$$\frac{D}{Dt} = \frac{\partial}{\partial t} + u \frac{\partial}{\partial x}. \quad (2.3)$$



- The Jacobian matrix of the flux $df(U)/dU$ has the eigenvalues

$$\lambda_1 = -C, \quad \lambda_2 = 0, \quad \lambda_3 = C, \quad (2.4)$$

- The Jacobian matrix of the flux $df(U)/dU$ has the eigenvalues

$$\lambda_1 = -C, \quad \lambda_2 = 0, \quad \lambda_3 = C, \quad (2.4)$$

where C denotes the Lagrangian sound velocity.

- For ideal gas

$$e = \frac{pV}{\gamma - 1}, \quad C^2 = \frac{\gamma p}{V}. \quad (2.5)$$

- For stiff fluid

$$e = \frac{(p + \gamma p_\infty)V}{\gamma - 1}, \quad C^2 = \frac{\gamma(p + p_\infty)}{V} \quad (2.6)$$



Finite volume method

- We divide the total mass into intervals of the length

$$\Delta\xi_i = \xi_{i+1/2} - \xi_{i-1/2}.$$

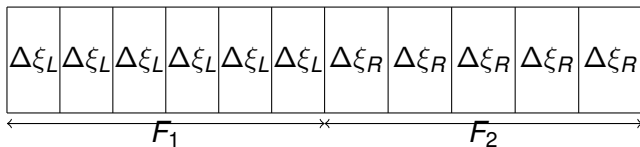


Figure: Setting up for one pair of layer

Finite volume method

- Integrating (2.1) over $[\xi_{i-1/2}, \xi_{i+1/2}]$ gives

$$\frac{d \langle U \rangle_i}{dt} + \frac{f(U(\xi_{i+1/2}, t)) - f(U(\xi_{i-1/2}, t))}{\Delta \xi_i} = 0, \quad (2.7)$$

where $\langle U \rangle_i = \frac{1}{\Delta \xi_i} \int_{\xi_{i-1/2}}^{\xi_{i+1/2}} U(\xi, t) d\xi$ and $f(U(\xi_{i+1/2}, t))$ is the flux evaluated at $\xi_{i+1/2}$.



Finite volume method

- Integrating (2.1) over $[\xi_{i-1/2}, \xi_{i+1/2}]$ gives

$$\frac{d \langle U \rangle_i}{dt} + \frac{f(U(\xi_{i+1/2}, t)) - f(U(\xi_{i-1/2}, t))}{\Delta \xi_i} = 0, \quad (2.7)$$

where $\langle U \rangle_i = \frac{1}{\Delta \xi_i} \int_{\xi_{i-1/2}}^{\xi_{i+1/2}} U(\xi, t) d\xi$ and $f(U(\xi_{i+1/2}, t))$ is

the flux evaluated at $\xi_{i+1/2}$.

We use $U_i \approx \langle U \rangle_i$ and replace $f(U(\xi_{i+1/2}, t))$ by the approximating numerical flux $F_{i+1/2}$.

- Second order (in space):

$$F_{i+1/2} = F(U_{i+1/2}^-, U_{i+1/2}^+). \quad (2.8)$$



- $U_{i+1/2}^-$ and $U_{i+1/2}^+$ can be reconstructed by using second order method with the minmod limiter:

$$U_{i+\frac{1}{2}}^- = U_i + U'_i \frac{\Delta \xi_i}{2}, \quad U_{i+\frac{1}{2}}^+ = U_{i+1} - U'_{i+1} \frac{\Delta \xi_{i+1}}{2}, \quad (2.9)$$

- $U_{i+1/2}^-$ and $U_{i+1/2}^+$ can be reconstructed by using second order method with the minmod limiter:

$$U_{i+1/2}^- = U_i + U'_i \frac{\Delta \xi_i}{2}, \quad U_{i+1/2}^+ = U_{i+1} - U'_{i+1} \frac{\Delta \xi_{i+1}}{2}, \quad (2.9)$$

- Minmod slope for 3 parameters

$$U'_i = 2MM \left(\frac{\theta(U_{i+1}^n - U_i^n)}{\Delta \xi_i + \Delta \xi_{i+1}}, \frac{U_{i+1}^n - U_{i-1}^n}{\Delta \xi_{i-1} + 2\Delta \xi_i + \Delta \xi_{i+1}}, \frac{\theta(U_i^n - U_{i-1}^n)}{\Delta \xi_{i-1} + \Delta \xi_i} \right)$$

where MM is the minmod limiter has the form

$\text{minmod3}(a, b, c) =$

$$\begin{cases} \min(|a|, |b|, |c|) \text{sign}(a) & \text{if } a, b, c \text{ have the same sign} \\ 0 & \text{if } a, b, c \text{ do not have the same sign} \end{cases}$$



High order (in time) numerical scheme

The equation (2.7) can be written as follows

$$\frac{dU_i}{dt} = - \frac{F_{i+1/2} - F_{i-1/2}}{\Delta\xi} =: \mathcal{F}_i. \quad (2.10)$$



Heun's method

We obtain the system of equations as follows

$$\frac{dU}{dt} = \mathcal{F} \quad (2.11)$$

where

$$U = \begin{pmatrix} U_1 \\ \vdots \\ U_N \end{pmatrix} \quad \text{and} \quad \mathcal{F} = \begin{pmatrix} \mathcal{F}_1 \\ \vdots \\ \mathcal{F}_N \end{pmatrix} \quad (2.12)$$

We will use Heun's method which is second order accurate in time and *strong stability-preserving*.



Heun's method

In order to generate a numerical solution, we follow 4 steps as follows

- Step 1 $K_1 = \mathcal{F}(U^n)$,
- Step 2 $\tilde{U} = U^n + \Delta t K_1$,
- Step 3 $K_2 = \mathcal{F}(\tilde{U})$,
- Step 4 $U^{n+1} = U^n + \Delta t(K_1 + K_2)/2$.



Roe Flux based on the composition of flux's jump

$$F_{newROE}(U_l, U_r) = \frac{1}{2} \left(F(U_l) + F(U_r) \right) - \frac{1}{2} \sum_{j=1}^3 \text{sign}(\lambda_j^{ROE}) \alpha_j r_j, \quad (2.13)$$



Roe Flux based on the composition of flux's jump

$$F_{newROE}(U_l, U_r) = \frac{1}{2} \left(F(U_l) + F(U_r) \right) - \frac{1}{2} \sum_{j=1}^3 \text{sign}(\lambda_j^{ROE}) \alpha_j r_j, \quad (2.13)$$

where α_j is the coefficient defined by solving the system

$$F(U_r) - F(U_l) = \sum_{j=1}^3 \alpha_j r_j. \quad (2.14)$$

This is the numerical flux obtained following Roe's idea by decomposing the flux instead of the conservative variables.

C. D. Munz. "On Godunov-Type Schemes for Lagrangian Gas Dynamics". In: *SIAM Journal on Numerical Analysis* 31.1 (Feb. 1994), pp. 17-42.



Outline

- 1 Problem setup
- 2 Detailed numerical solution
- 3 Numerical tests**
- 4 Multi-fluid models
- 5 Numerical comparison

Multi-layer tube

We consider a tube filled by n_p pairs of layers, each pair consists of 2 layers of 2 different fluids.

The initial condition for the velocity u , pressure denoted by p

and the initial density satisfies $\rho = \bar{\rho} \left(\frac{p+p_\infty}{\bar{p}+p_\infty} \right)^{\frac{1}{\gamma}}$, \bar{x} is the middle point of the domain with length of 10, $\bar{p} = p_{10} = p_{20} = 10$ and $\bar{\rho}$ is $\rho_{10} = 20$ or $\rho_{20} = 10$, p_∞ is stiffness parameter, $p_{\infty 1} = 100$, $p_{\infty 2} = 0$, $\gamma_1 = 4.4$ and $\gamma_2 = 1.4$ corresponding to the position in the tube.



Wave interaction among small number of layers

We consider a tube with $n_p = 5$ and the following initial condition

$$\begin{cases} p_L = 40, u_L = 0.9452, & \text{if } 0 \leq x \leq 1 \\ p_R = 10, u_R = 0, & \text{if } 1 < x \leq 10, \end{cases} \quad (3.1)$$

and the initial density satisfies $\rho = \bar{\rho} \left(\frac{p + p_\infty}{\bar{p} + p_\infty} \right)^{\frac{1}{\gamma}}$.



Wave interaction among small number of layers

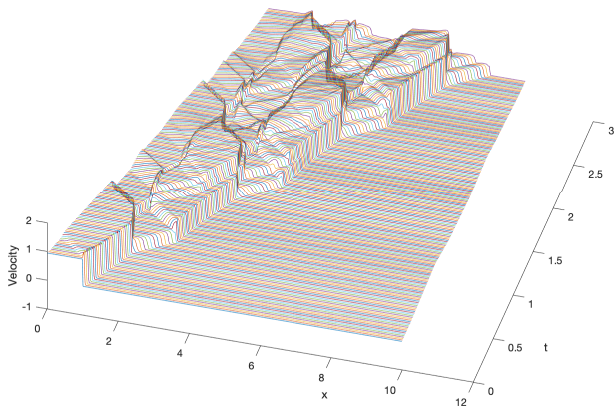


Figure: Velocity profiles of shock propagating in the tube from the initial time up to final time $T_{final} = 3$. Result is plotted in **Eulerian coordinates**

Wave interaction among small number of layers

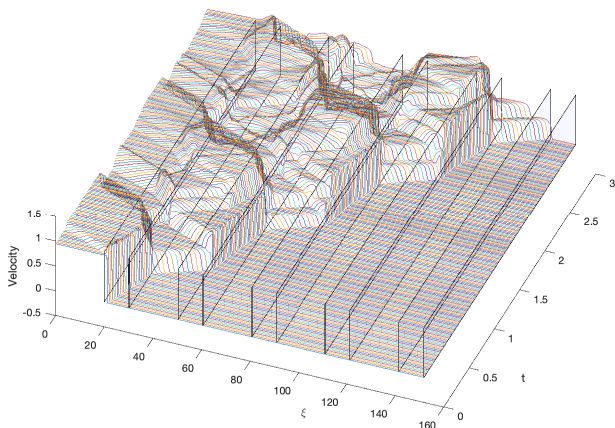


Figure: Velocity profiles of shock propagating in the tube from the initial time up to final time $T_{final} = 3$. Result is plotted in **Lagrangian coordinates**



Wave interaction among small number of layers

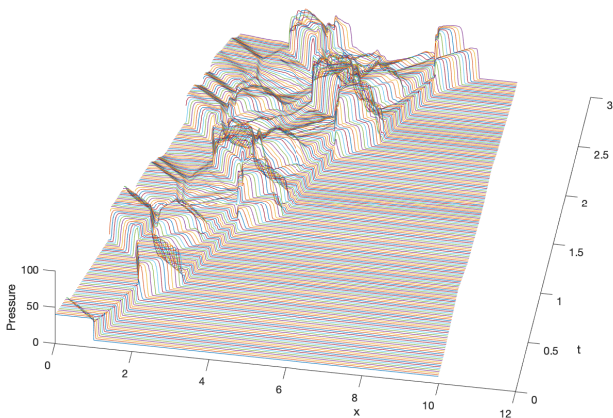


Figure: Pressure profiles of shock propagating in the tube from the initial time up to final time $T_{final} = 3$. Result is plotted in **Eulerian coordinates**

Wave interaction among small number of layers

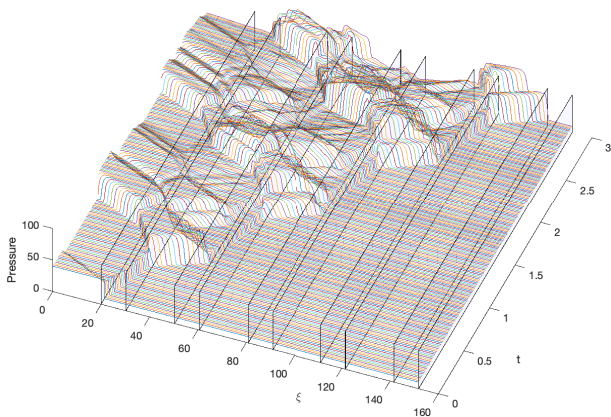


Figure: Pressure profiles of shock propagating in the tube from the initial time up to final time $T_{final} = 3$. Result is plotted in **Lagrangian coordinates**

Wave interaction among small number of layers

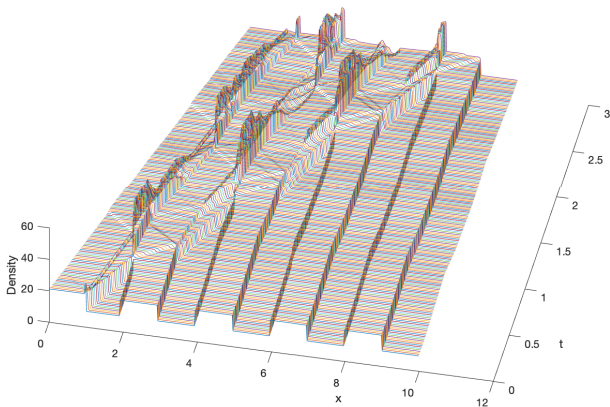


Figure: Density profiles of shock propagating in the tube from the initial time up to final time $T_{final} = 3$. Result is plotted in **Eulerian coordinates**

Wave interaction among small number of layers

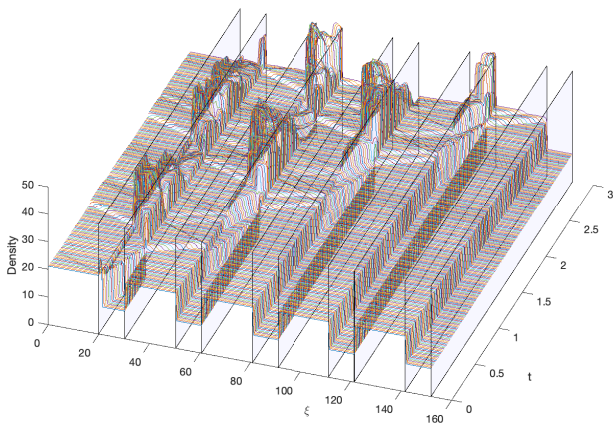


Figure: Density profiles of shock propagating in the tube from the initial time up to final time $T_{final} = 3$. Result is plotted in **Lagrangian coordinates**

We consider a initial condition with velocity is zero, a smooth pressure profile of the form

$$\begin{cases} \rho = 10 + M \left(1 + \cos \left(\frac{2\pi(x-\bar{x})}{L} \right) \right), & \text{if } |x - \bar{x}| < L/2 \\ \rho = 10, & \text{if } |x - \bar{x}| \geq L/2 \end{cases} \quad (3.2)$$

and the initial density satisfies $\rho = \bar{\rho} \left(\frac{\rho + \rho_\infty}{\bar{\rho} + \rho_\infty} \right)^{\frac{1}{\gamma}}$.



Initial condition with $M = 5$, $L = 5$.

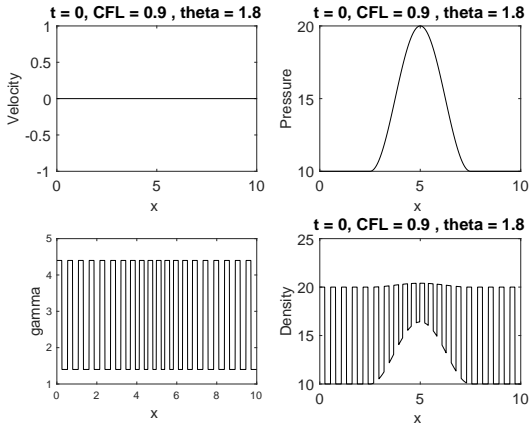


Figure: Initial condition.

Result with $M = 5$, $L = 5$. Numerical flux: Roe Flux based on the composition of flux's jump

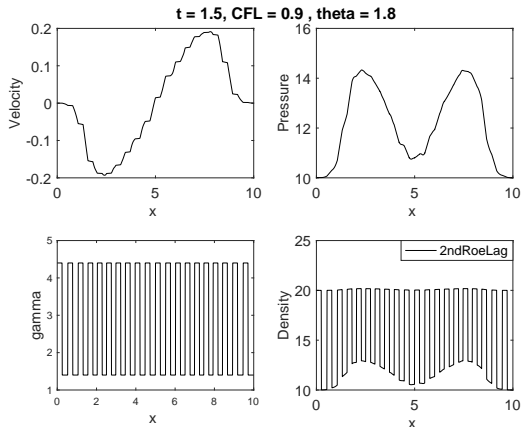


Figure: Result with 20 pairs of layers, 50 points for each pair.



Outline

- 1 Problem setup
- 2 Detailed numerical solution
- 3 Numerical tests
- 4 Multi-fluid models**
- 5 Numerical comparison

Isentropic homogeneous model (2x2 model)

Considering isentropic Euler equations corresponding to the conservation of mass and momentum in Lagrangian coordinates

$$\begin{cases} V_t - u_\xi = 0 \\ u_t + p_\xi = 0, \end{cases} \quad (4.1)$$

Relation $V = V(p)$ for the mixture

$$V = Y_1 V_{10} \left(\frac{p + p_{\infty,1}}{p_{10} + p_{\infty,1}} \right)^{-\frac{1}{\gamma_1}} + Y_2 V_{20} \left(\frac{p + p_{\infty,2}}{p_{20} + p_{\infty,2}} \right)^{-\frac{1}{\gamma_2}}, \quad (4.2)$$

where Y_1 and Y_2 are the mass fraction of each phase.



3x3 system with turbulent energy

The system in Lagrangian form

$$\begin{cases} V_t - u_\xi = 0, \\ u_t + \tilde{p}_\xi = 0, \\ \epsilon_t + (u\tilde{p})_\xi = 0, \end{cases} \quad (4.3)$$

where $V = \frac{1}{\rho}$, $\epsilon = e + \frac{u^2}{2} + Vk$, $\tilde{p} = p + 2k$ and $e = Y_1 e_1 + Y_2 e_2$ is the specific internal energy of the mixture,

$$e_1 = \frac{p + \gamma_1 p_{\infty 1} L}{\gamma_1 - 1} V_1, \quad e_2 = \frac{p + \gamma_2 p_{\infty 2}}{\gamma_2 - 1} V_2. \quad (4.4)$$

S. L. Gavriluk and R. Saurel. "Rankine-Hugoniot relations for shocks in heterogeneous mixtures". In: *Journal of Fluid Mechanics* 575 (Mar. 2007), pp. 495-507.



Outline

- 1 Problem setup
- 2 Detailed numerical solution
- 3 Numerical tests
- 4 Multi-fluid models
- 5 Numerical comparison**

Data for two cases

- Case 1: $\rho_{10}/\rho_{20} = 2$
- Case 2: $\rho_{10}/\rho_{20} = 10$

Reference data	Case 1	Case 2
ρ_{10}	10	10
ρ_{10}	20	100
$\rho_{\infty,1}$	100	100
γ_1	4.4	4.4
ρ_{20}	10	10
ρ_{20}	10	10
$\rho_{\infty,1}$	0	0
γ_2	1.4	1.4

Table: Reference states of the multilayer tube



Numerical results before shock formation

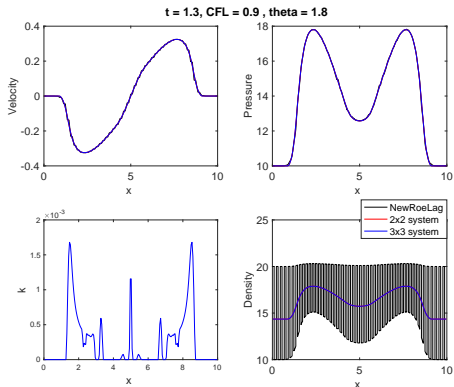


Figure: Comparison between numerical solution of multi-fluid and homogeneous models before shock formation for the case of density ratio $\rho_{10}/\rho_{20} = 2$ at time $t = 1.3$.

Numerical results before shock formation

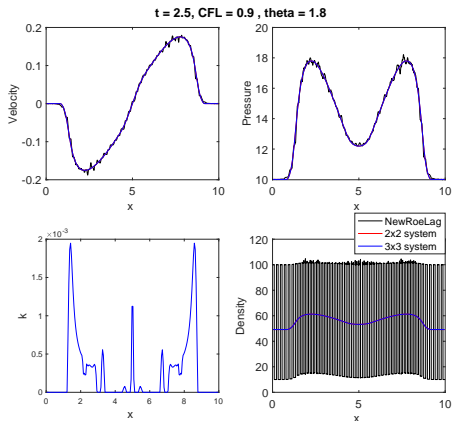


Figure: Comparison between numerical solution of multi-fluid and homogeneous models before shock formation for the case of density ratio $\rho_{10}/\rho_{20} = 10$ at time $t = 2.5$.

Numerical results after shock formation

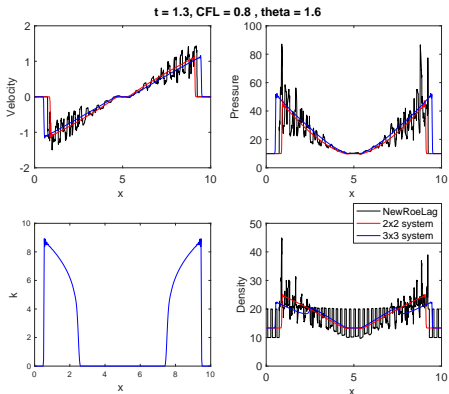


Figure: Comparison between numerical solution of multi-fluid and homogeneous models after shock formation for the case of density ratio $\rho_{10}/\rho_{20} = 2$ at time $t = 1.3$ (strong shock).

Using Gaussian blurring to smooth out numerical solutions

$$U_i = \frac{1}{2}(U_{i-1} + U_{i+1}). \quad (5.1)$$



Numerical results after shock formation

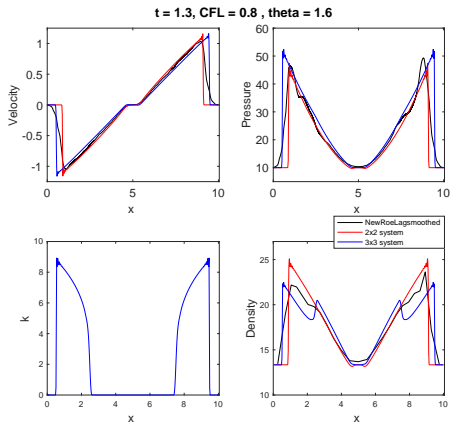


Figure: Comparison between smoothed numerical solution of multi-fluid and homogeneous models for the case of density ratio $\rho_{10}/\rho_{20} = 2$.

Numerical results after shock formation

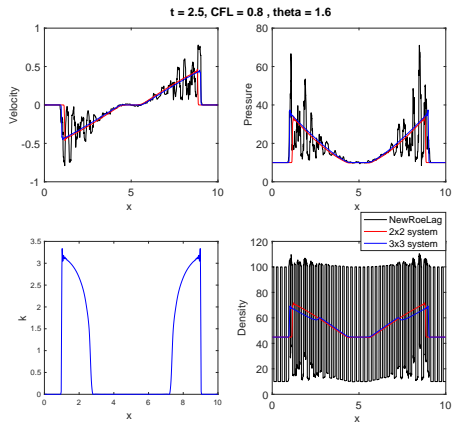


Figure: Comparison between numerical solution of multi-fluid and homogeneous models after shock formation for the case of density ratio $\rho_{10}/\rho_{20} = 10$ at time $t = 2.5$ (strong shock).

Numerical results after shock formation

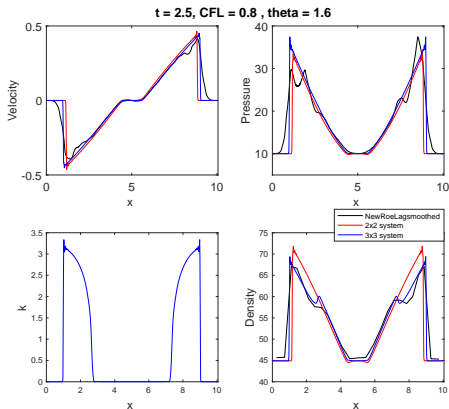


Figure: Comparison between smoothed numerical solution of multi-fluid and homogeneous models for the case density ratio $\rho_{10}/\rho_{20} = 10$.

Riemann problem for multi-fluid

We consider the test with the following initial condition for the pressure

$$p = \begin{cases} 50, & \text{if } x \leq 5 \\ 10, & \text{if } x > 5, \end{cases} \quad (5.2)$$

where $x \in [0, 10]$. The initial velocity is zero everywhere and the initial density satisfies $\rho = \bar{\rho} \left(\frac{p + p_\infty}{\bar{p} + p_\infty} \right)^{\frac{1}{\gamma}}$. For the 3×3 model k is also zero.



Riemann problem for multi-fluid

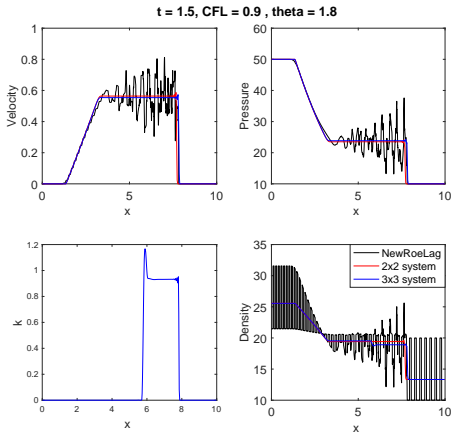


Figure: Comparison between detailed numerical solution of multi-fluid and homogeneous models of Riemann problem (5.2) for the case of density ratio $\rho_{10}/\rho_{20} = 2$ at time $t = 1.5$.



Riemann problem for multi-fluid

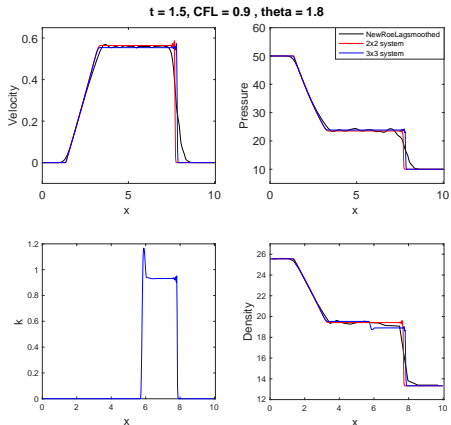


Figure: Comparison between smoothed numerical solution of multi-fluid and homogeneous models of Riemann problem (5.2) for the case of density ratio $\rho_{10}/\rho_{20} = 2$ at time $t = 1.5$.

Riemann problem for multi-fluid

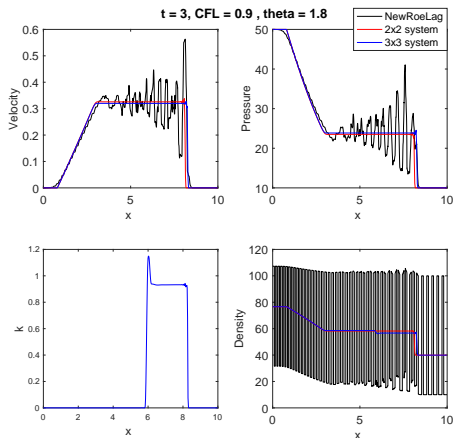


Figure: Comparison between detailed numerical solution of multi-fluid and homogeneous models of Riemann problem (5.2) for the case of density ratio $\rho_{10}/\rho_{20} = 10$ at time $t = 3$.

Riemann problem for multi-fluid

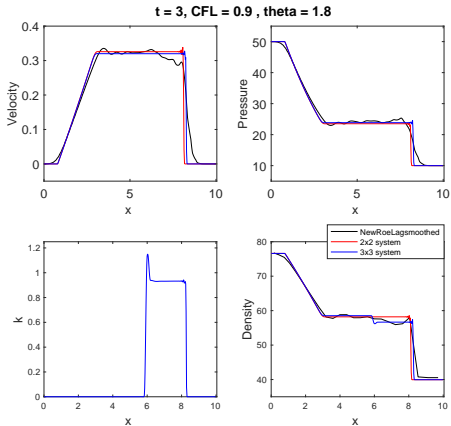


Figure: Comparison between smoothed numerical solution of multi-fluid and homogeneous models of Riemann problem (5.2) for the case of density ratio $\rho_{10}/\rho_{20} = 10$ at time $t = 3$.



Travelling shock - moderate density ratio

The initial condition of the travelling shock for 2×2 system is

$$\begin{cases} \rho_L = 40, u_L = 0.9452, & \text{if } 0 \leq x \leq 1 \\ \rho_R = 10, u_R = 0, & \text{if } 1 < x \leq 10, \end{cases} \quad (5.3)$$

and the initial density satisfies $\rho = \bar{\rho} \left(\frac{\rho + \rho_\infty}{\bar{\rho} + \rho_\infty} \right)^{\frac{1}{\gamma}}$.

At $x = 10$ we impose wall conditions : $u = 0, \partial p / \partial \xi = 0$.



Numerical results before hitting the wall

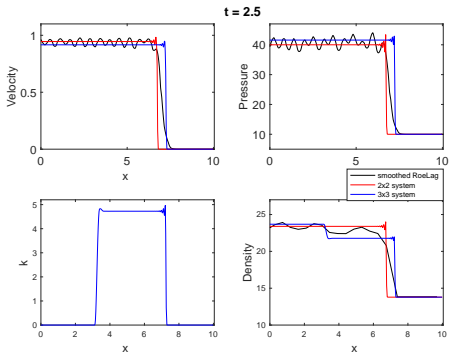


Figure: Comparison between smoothed detailed numerical solution, 2×2 system, 3×3 system before hitting the wall for the case of density ratio $\rho_{10}/\rho_{20} = 2$ at time $t = 2.5$.

Numerical results after hitting the wall

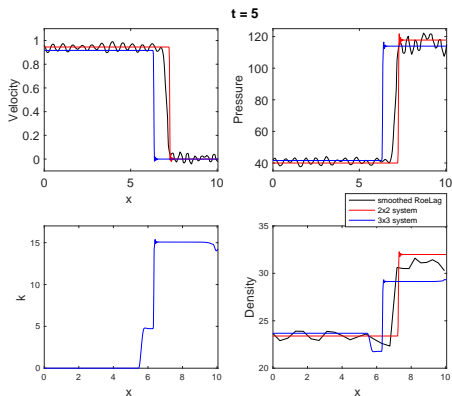


Figure: Comparison between smoothed detailed numerical solution, 2×2 system, 3×3 system after hitting the wall for the case of density ratio $\rho_{10}/\rho_{20} = 2$ at time $t = 5$.

Travelling shock - big density ratio

The initial condition of the Riemann problem is

$$\begin{cases} \rho_L = 40, u_L = 0.5286, & \text{if } x \leq 1 \\ \rho_R = 10, u_R = 0, & \text{if } x > 1, \end{cases} \quad (5.4)$$

where $x \in [0, 10]$.

The initial density satisfies $\rho = \bar{\rho} \left(\frac{\rho + \rho_\infty}{\bar{\rho} + \rho_\infty} \right)^{\frac{1}{\gamma}}$.



Numerical results before hitting the wall

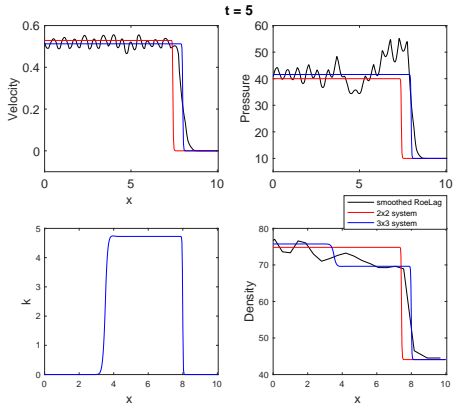


Figure: Comparison between smoothed detailed numerical solution, 2×2 system, 3×3 system before hitting the wall for the case of density ratio $\rho_{10}/\rho_{20} = 10$ at time $t = 5$.



Numerical results after hitting the wall

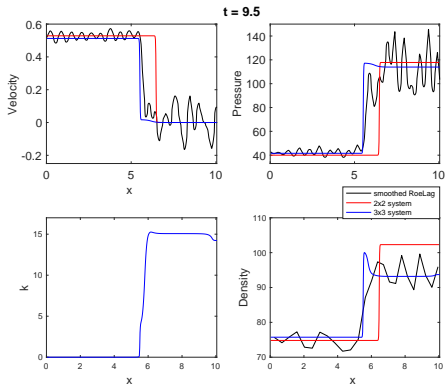


Figure: Comparison between smoothed detailed numerical solution, 2×2 system, 3×3 system after hitting the wall for the case of density ratio $\rho_{10}/\rho_{20} = 10$ at time $t = 9.5$.



Comparison of the computation time

Detailed computation	2×2 system	3×3 system
298.8	42.8	50.1

Table: Comparison of the computation time (seconds) among the computations of the detailed numerical solution and the two homogeneous models

Conclusion: It is much more expensive to perform the detailed numerical simulation than to numerically solve the homogeneous models.



Discussion and conclusion

- For smooth solutions (in pressure and velocity) the two models are both in very good agreement with the detailed numerical solution of multilayer Euler equations.
- When a shock develops, the multilayer solution becomes highly oscillatory and transforms to a dispersive shock for large amplitude shocks.
 - For moderate density ratio, the 2×2 model gives a better prediction of the shock position.
 - For large density ratio, the turbulent 3×3 model is in better agreement with a smoothed out version of the detailed numerical compared with the simple 2×2 model.
- Open problem: construction of non isentropic homogenized models.



Reference

D.T. M. Phan, S.L. Gavriluk and G. Russo, "Numerical validation of homogeneous multi-fluid models", *Applied Mathematics and Computation* 441 (2023) 127693
<https://doi.org/10.1016/j.amc.2022.127693>



Thank you for your attention!